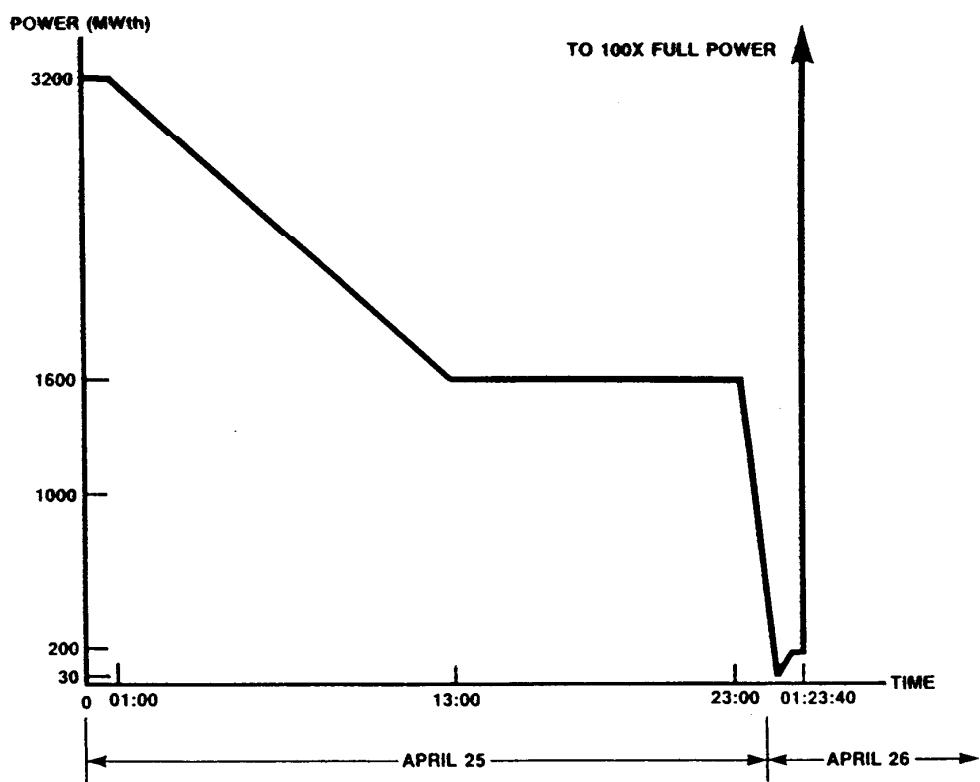


1986-10-10
10:10

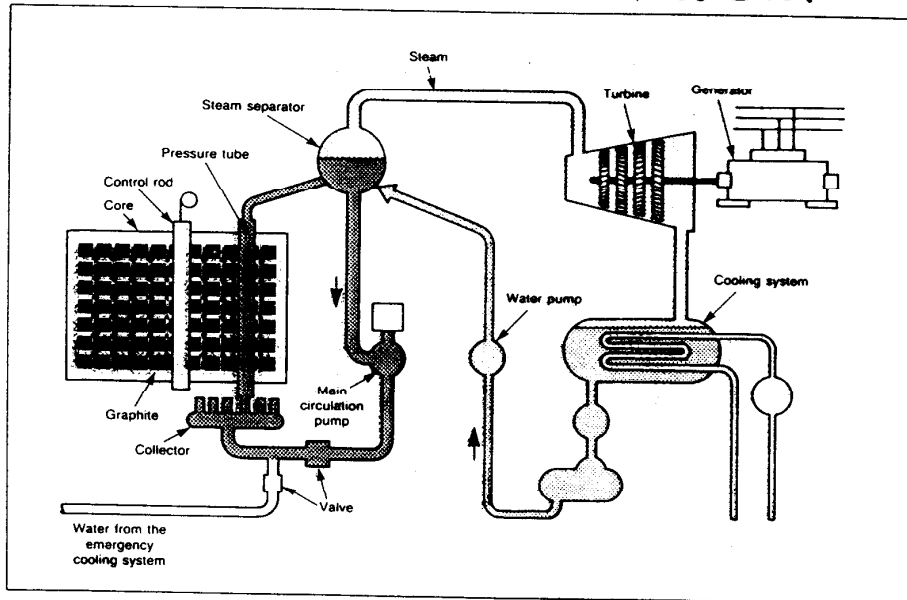
CHERNOBYL: A TRAGEDY OF ERRORS

Jeremy Whitlock
AECL

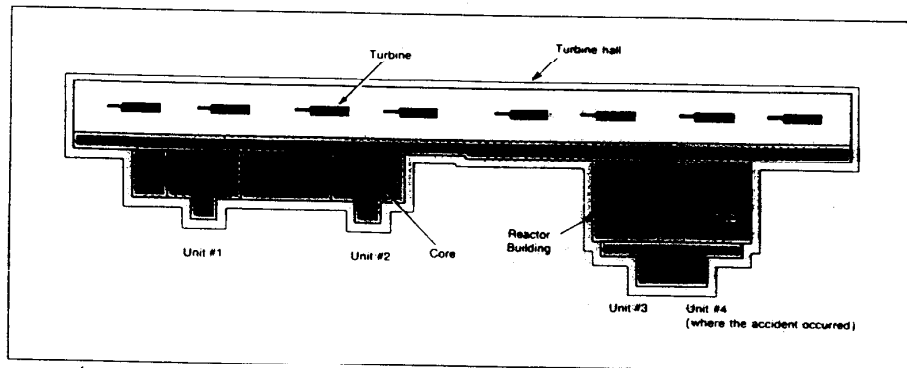


RBMK-1000:

"Heterogeneous
Water-Graphite
Channel-Type
Reactor"

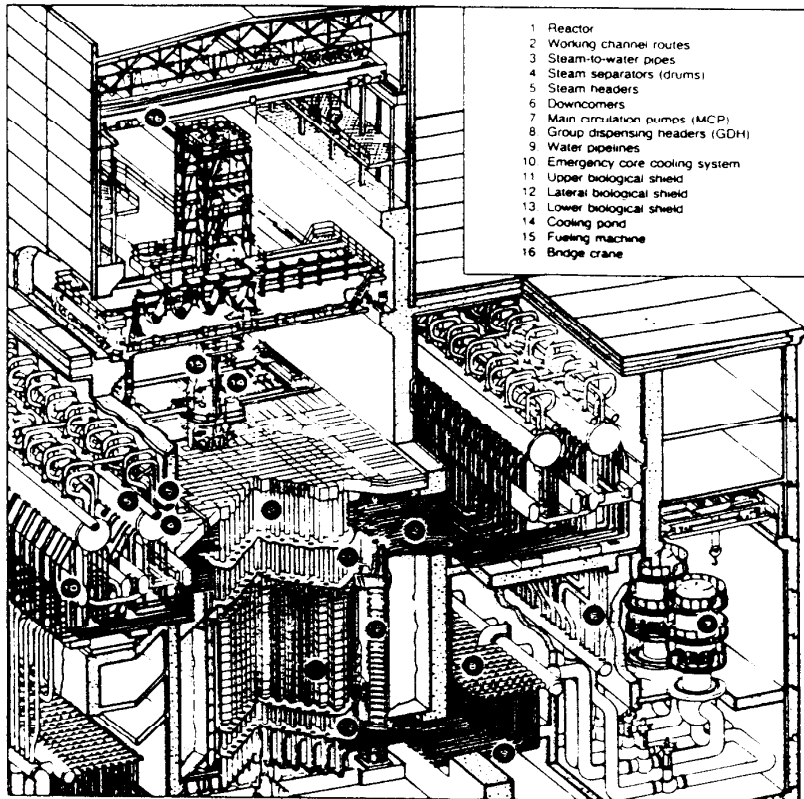


Schematic diagram of the RBMK-1000

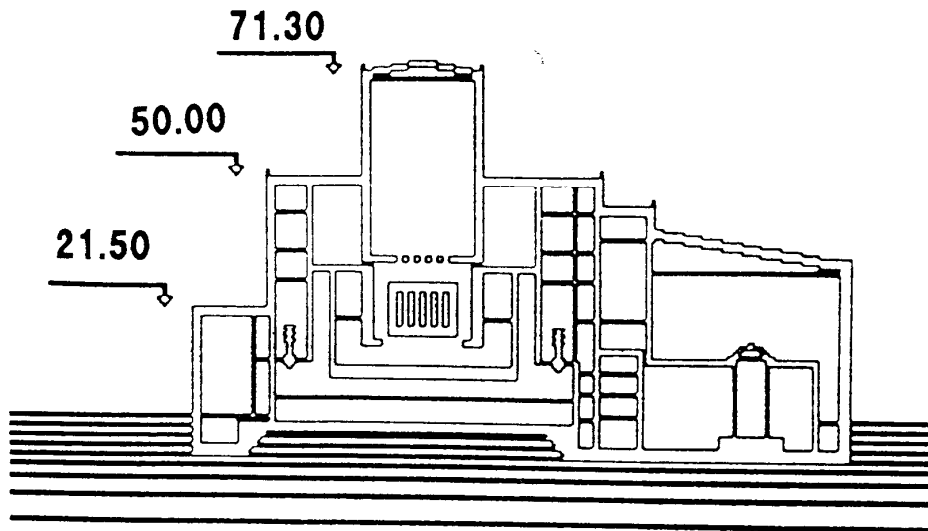


Layout of four reactor units

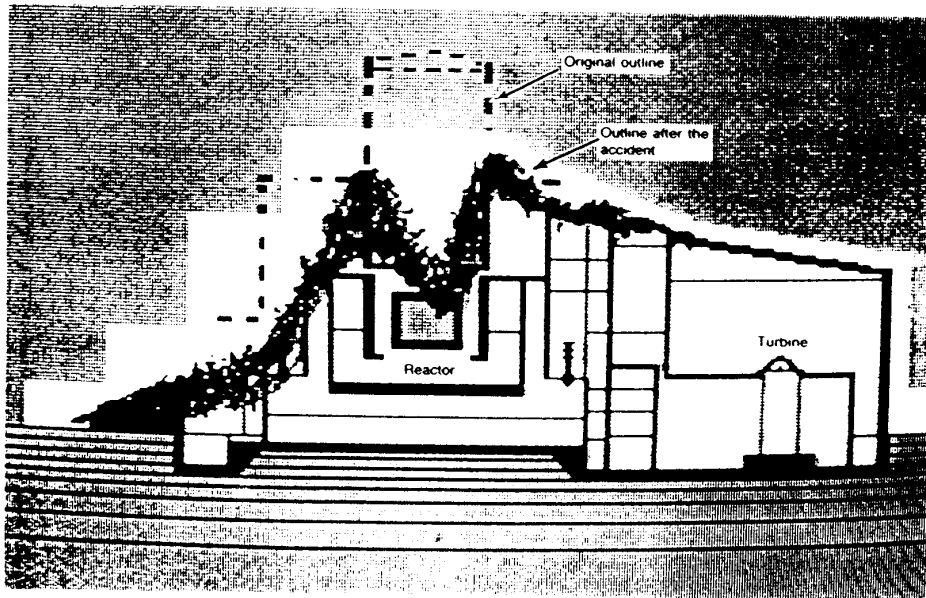
- 3200 MWth (1000 MWe)
- core: 7m high, 12m diameter
- 1661 fuel channels
- fuelled on-line
- direct cycle, steam mass quality 11-22%
- 2 loops, 3 pumps/loop + 1 standby pump/loop



FUEL	COOLANT	MODERATOR
2% enriched	light water	graphite
UO_2	$P = 7 \text{ MPa}$	$T = 700^\circ\text{C}$
2 subassemblies per channel	$T_{\text{out}} = 285^\circ\text{C}$	$\alpha_T = +.06/^\circ\text{C}$ (slow)
18 pins per subassembly	avg. steam fraction 14.5%	
fuel pin 13.5 mm diameter	$\alpha_v = +.05/\% \text{ void}$	
$\alpha_T = -.02 \text{ mk}/^\circ\text{C}$		



VIEW OF THE REACTOR BEFORE THE ACCIDENT



VIEW OF THE DAMAGED REACTOR

CONTROL PROBLEMS

- at low power, small flow deviations cause large power fluctuations.
- hard to match flow and power levels at low power.
- detector feedback slow.
- control rod insertion slow (~ 20 sec.).
- spatial modes easily incited \rightarrow less than 10% core needed for criticality; first azimuthal harmonic only 6-7.5 mk subcritical.
- significant Plutonium build-up leads to low β -values (β for $\text{Pu}^{239} = 2.2 \times 10^{-3}$
 β for $\text{U}^{235} = 6.9 \times 10^{-3}$)
- operation therefore not "permitted" below 20% power, and min. reactivity insertion ~ 30 rods $\rightarrow \alpha_v$ at these bounds is $\frac{.2 \text{mk}}{\% \text{void}}$

SHUTDOWN

- 24 emergency rods (only system)
- effectiveness dependent on reactor operating conditions — mainly # of control rods in core and power-flow match.
- slow insertion rate.

APRIL 25, 1986

The Experiment

- design-basis accident: loss of coolant plus loss of off-site power
- reactor trips, ECC pumps powered by turbine inertia until diesels start up (~60 sec.)
- test of new voltage regulator:
 - ① power reduction → 700-1000 MWth.
 - ② trip one of two turbines; transfer all steam to other turbine.

cont'd...

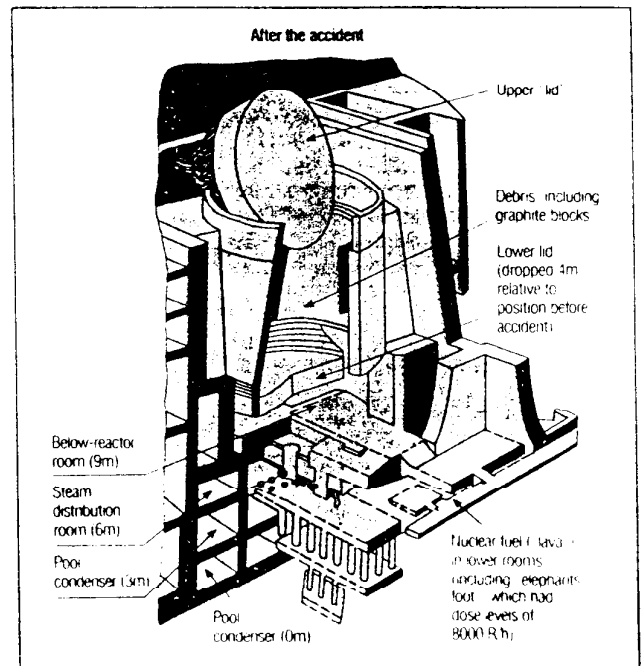
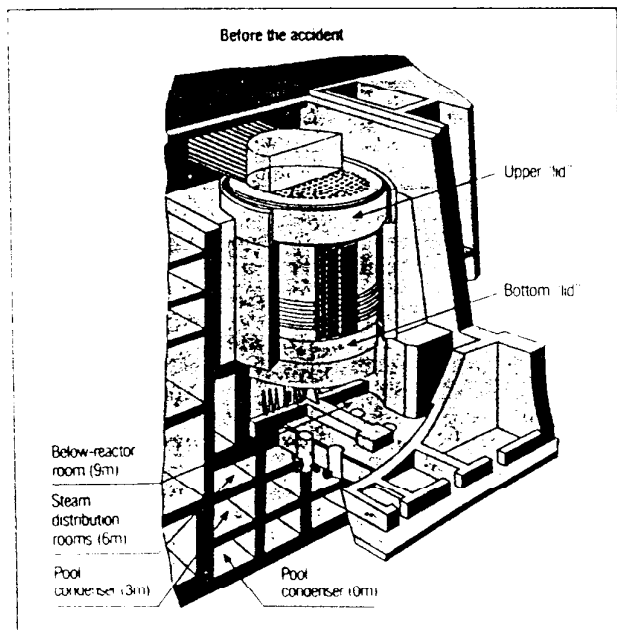
- ③ start extra pump in each loop.
- ④ disconnect ECC .
- ⑤ trip remaining turbine ; observe voltage rundown .

The Events

TIME	REL. TIME	EVENT
~APRIL 25~ 1:00 am	0:00	Begin power reduction .
1:05 pm	12:05	Reactor at 50% power . One turbine tripped .
2:00 pm	13:00	ECC disconnected . "Hold-power" request received . ECC unavailable
11:10 pm	22:10	Power rundown continued .
~APRIL 26~ 12:28 am	23:28	Switch from "local" to "bulk" control . ERROR: Set point incorrectly set ; Power falls to 30 MWth (~1% power) . RESULT: Xenon poisoning ; α_v increased ; reactor in unstable regime .
1:00 am	24:00	Power raised to 200 MWth (6% power) . ERROR: Reactivity margin reduced to below 30 rods . RESULT: Increased α_v , instability .

TIME	REL.TIME	EVENT
1:07 am	24:07	Fourth (standby) pump in each loop started. Flow rate exceeds safe limit. Further void collapse causes drop in system pressure, separator level.
1:19 am	24:19	Feedwater flow increased to raise separator level. T_{in} decreases \rightarrow further void collapse.
1:19:30 am	24:19:30	Separator level rises too high. Automatic control rods rise to limit. Manual rods raised to return auto. rods to operating region.
1:19:58 am	24:19:58	Condenser steam dump valve closed.
1:21:50 am	24:21:50	Feedwater flow abruptly reduced.
1:22:10 am	24:22:10	Steam quality begins to increase. Automatic rods lower.
1:22:30 am	24:22:30	Feedwater flow reduction stopped. Power distribution, reactivity margin printed out \rightarrow 6-8 rods in core, flux "double humped".
1:22:45 am	24:22:45	Steam quality stabilizes. Pseudo-steady-state observed.
1:23:04 am	24:23:04	DECISION TO BEGIN TEST. Second turbine tripped. ERROR: Reactor "loss-of-turbine" trip blocked. RESULT: 200 MWth operation.

TIME	REL. TIME	EVENT
1:23:21 am	24:23:21	Automatic rods lower due to void-induced reactivity increase. Void determined by increasing pressure (-), decreasing pump speed (+), low feedwater flow (+). Net effect: +
1:23:31 am	24:23:31	Power begins to rise.
1:23:40 am	24:23:40	Manual trip button pushed. Rods drop 2-2.5 m into core, and stop. Power surges to ~100X in 4 seconds.
1:23:48 am	24:23:48	Steam explosion, followed seconds later by second explosion (H_2 , CO igniting with air).



▲ Chernobyl unit 4: before and after.

The Results

- Reactor building blown away. ~30 fires on turbine hall roof, put out by 5:00 am.
- Graphite fire drives updraft for 10 days. Put out by dumping ~5000 tonnes of boron, lead, dolomite, sand, clay on core, with N_2 injection. ~10% of total (250 tonnes) burns.
- ~3.5% fuel inventory dispersed in vicinity.
- ~50 MCi noble gases + 50 MCi other species dispersed around northern hemisphere.
- ~20,000 extra fatal cancers in northern hemisphere (half in U.S.S.R.).
- 31 immediate deaths (operators, firefighters).
- units 1, 2 & 3 still operate.

CHERNOBYL

VOID COEFFICIENT

H₂O Coolant

- large absorption $\rightarrow \rho$ increases on voiding
- scattering effects (decrease in moderation; increase in "p" factor) are small.

Graphite Moderator

- moderator hotter than coolant (700°C/285°C)
- loss of extra neutron "cooling" on voiding increases avg. Maxwellian temp \rightarrow
- U²³⁵ reaction rate decreases, Pu²³⁹ rate increases (0.3 eV resonance)
- net effect $\rightarrow \rho$ increases on voiding for high burnup fuel; decreases for fresh fuel.

Absorber Rods

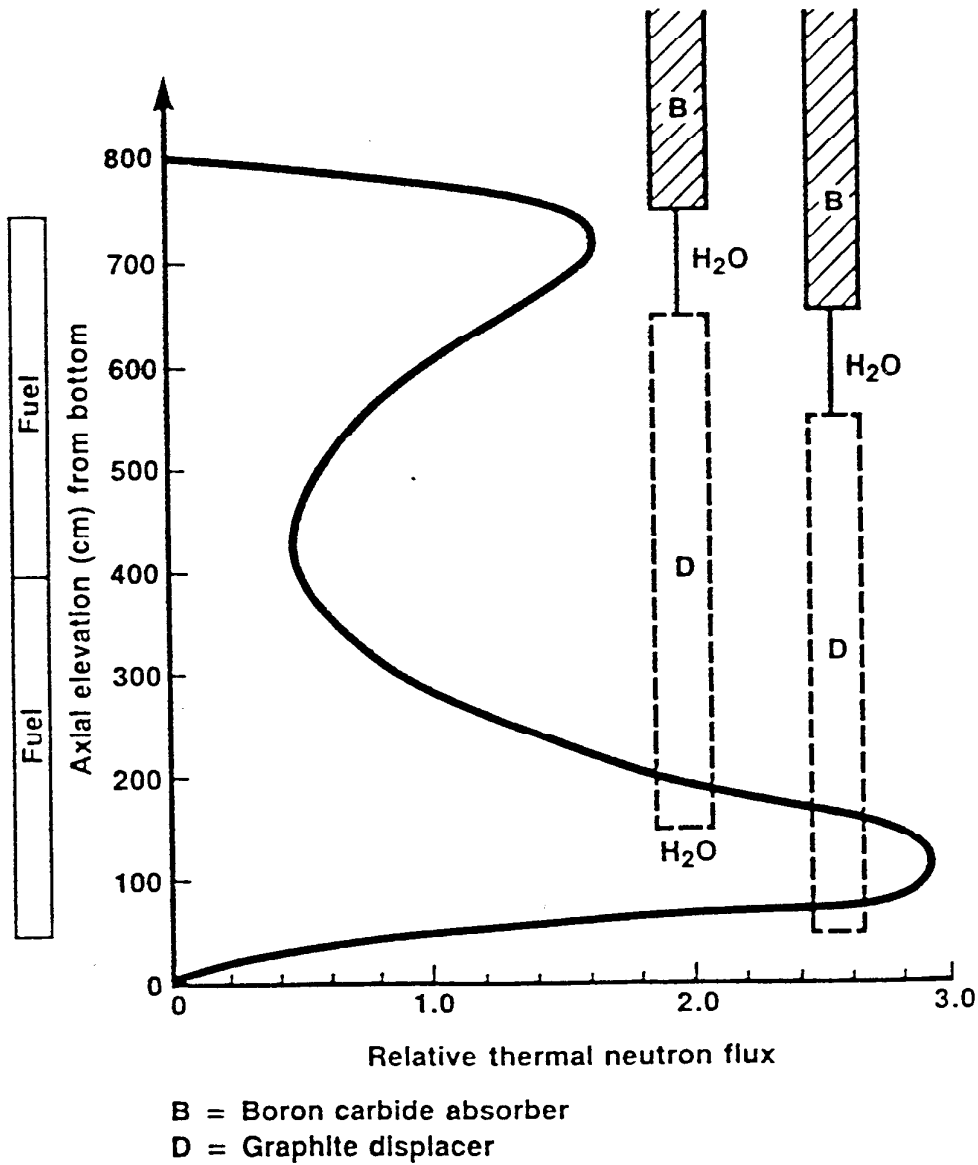
- used to reduce void reactivity (80 rods) ($\rightarrow 0.05 \text{ mk}/\%$)
- minimum 30 rods required partially (1.2m) in core. ($0.2 \text{ mk}/\%$)

Direct Cycle

- significant operational void levels (14.5%)
 - low power \rightarrow low void $\rightarrow \alpha_v \approx 0.2 \text{ mk}/\%$ void
- \therefore problem at low power and min rod insertion

"POSITIVE SCRAM"

AXIAL FLUX DISTRIBUTION
PRECEDING ACCIDENT



PROPOSED CHANGES

Short Term

- Minimum rod insertion changed to 80 rods
- Limit stop switch on control rods, set for 1.2 m.
- Better knowledge of operating rules.*

Long Term

- Increase enrichment from 2.0% to 2.4%
- Faster, more independent shutdown system.
- Reactivity monitor, with reactor trip.
- Other operator info. (eg. dryout margin) more readily available.
- Longer graphite follower on control rods.
- Harder to over-ride automatic controls.

Lingering Questions ...

- Still inferior to Western plants.
- Initiating events → positive scram?
→ thermal shocks?
→ pump cavitation?

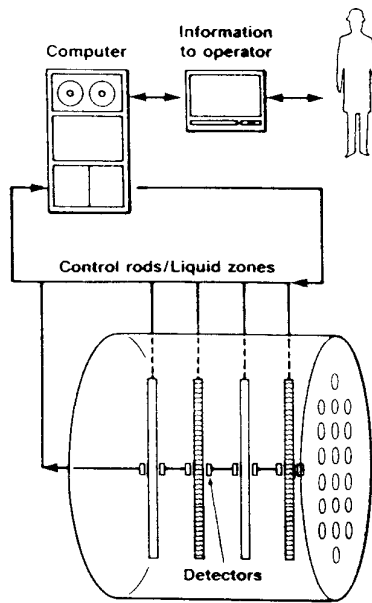
COMPARISON OF CHERNOBYL REACTOR
WITH BRUCE-B REACTOR

	<u>CHERNOBYL</u>	<u>BRUCE-B</u>
Type	RBMK	CANDU
Thermal Power, MW	3200	2852
Moderator	Graphite 700°C	Heavy water 80°C
Coolant	Water (boiling, $x_o = 14\%$) 285°C	Heavy water 290°C
Cycle	Direct	Indirect
Fuel	UO_2 -2% enriched	UO_2 -natural
Orientation	Vertical	Horizontal
Core Outlet Pressure, MPa	7	9.3
Pressure Containment.	Pressure Tubes (Zr Nb)	Pressure Tubes (Zr Nb)
Number of Fuel Channels	1660	480
Core Diameter, m	11.8	7.07
Core Height or Length, m	7.0	5.94
Re-fuelling	On power	On power
Equilibrium max. void reactivity	20 mk ($\sim 400\%$ change with power)	11 mk (\sim constant with power)
Shutdown	20 seconds	2 seconds

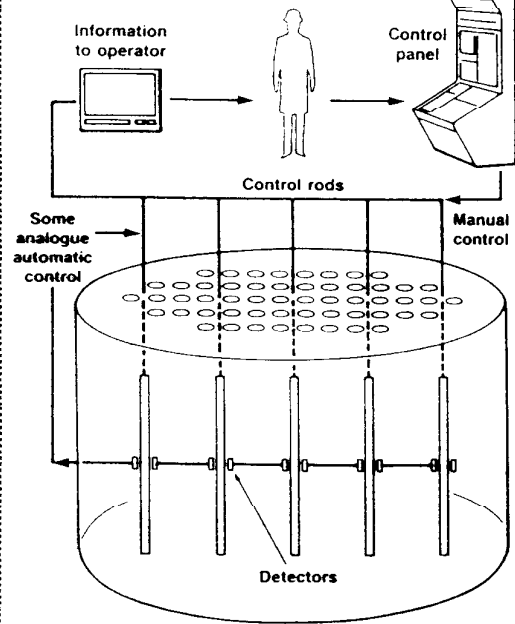
Mitigating factors in CANDU :

better training, faster shutdown, better spatial & temporal control, containment, heavy water moderator, control & shutdown independent of operating parameters, double (independent) shutdown systems.

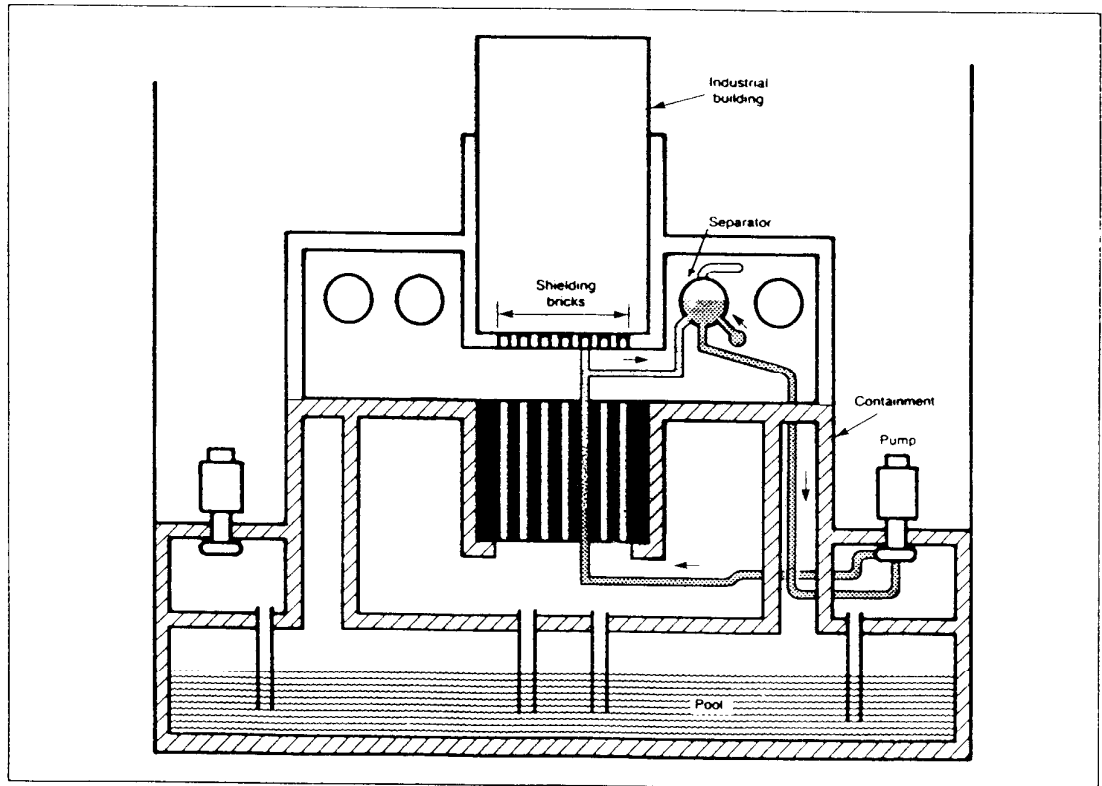
ROUTINE
CANDU CONTROL



ROUTINE
CHERNOBYL CONTROL



CONTROLLING THE POWER



Chernobyl containment