



CANDU Safety

#23 - Regulatory Requirements for Accident Analysis

Dr. V.G. Snell
Director
Safety & Licensing



Review of Safety Philosophy

- λ goal-oriented, not prescriptive
 - up to designer to define complete set of accidents
- λ risk-based origins
 - accident classes and dose limits based on frequency
- λ deterministic requirements for design basis accidents
 - accident analysis uses conservative input data & assumptions
- λ physically-based system models
- λ reference document: AECB Consultative Document C-6 Rev. 0
 - used in Darlington and beyond (Wolsong, Qinshan)



Purpose of Safety Analysis

- λ from designer point of view:
 - to assist in the design
 - to identify any safety design deficiencies
 - to ensure that the safety systems meet performance requirements
- λ from the regulatory point of view:
 - safety analysis is a way of testing the adequacy of the safety aspects of the design
 - provides evidence of acceptable risk to the public



Definition

- λ *serious process failure* - failure of any process equipment which in the absence of special safety system action could result in significant fuel failures in the reactor or a significant release of radioactive material from the station
- λ these are serious process failures:
 - large loss of coolant
 - loss of reactivity control stopped by the shutdown systems
 - single channel flow blockage
- λ these are *not* serious process failures:
 - loss of reactivity control stopped by stepback
 - loss of primary side pressure control - high



Process

- λ identify design basis accidents (systematic plant review)
- λ perform accident analysis
- λ compare results to acceptance criteria:
 - public dose: set by AECB
 - other criteria:
 - λ some set by AECB - e.g., no fuel failures for small LOCA
 - λ some set by designer: e.g., no calandria tube dryout for LOCA with loss of Emergency Core Cooling



Systematic Plant Review

- λ designers must identify all design basis accidents through systematic review:
 - all serious process failures resulting from failure of a single component or system, or combinations thereof
 - all serious process failures combined with failure or unavailability of mitigating systems
 - the frequency of all such events
- λ minimum list of events given as a starting point



Event Classes

- λ events and event combinations divided into 5 classes
- λ based approximately on frequency
- λ permissible dose increases with decreasing frequency
- λ AECB does not specify frequency but it can be inferred from their minimum list of events
- λ events identified by designer are put in the same class as events of similar frequency



Dose Limits

<i>Class</i>	<i>Whole Body Dose Limit (Sv)</i>	<i>Thyroid Dose Limit (Sv)</i>
<i>1</i>	0.0005	0.005
<i>2</i>	0.005	0.05
<i>3</i>	0.03	0.3
<i>4</i>	0.1	1
<i>5</i>	0.25	2.5



Class 1 - Examples

- λ loss of reactivity control**
- λ loss of Class IV electrical power**
- λ loss of main feedwater flow**
- λ loss of service water flow**
- λ loss of instrument air**
- λ loss of moderator flow**
- λ fuelling machine backing off reactor without replacing closure plug**
- λ failure of instrument line**
- λ fail open of heat transport system pressure relief valve**
- + *i.e., expected to occur once or so during plant operation***



Class 2 - Examples

- λ feeder pipe break
- λ end-fitting failure
- λ pressure-tube failure + *assumed* calandria tube failure
- λ flow blockage of a fuel channel
- λ single heat transport system pump seizure
- λ pressure and inventory control system failures
- λ service water pipe failures
- λ design basis fires
- + *i.e., expected to occur less than once during plant operation*



Class 3 - Examples

- λ large LOCA
- λ steam main pipe break
- λ feedwater pipe break
- λ design basis earthquake
- λ moderator pipe break
- + *i.e., events expected to occur less than once per thousand years*



Class 4 - Examples

- λ fuelling machine backing off reactor without replacing closure plug and, in turn:
 - loss of Emergency Core Coolant injection
 - heat transport system loop isolation failure
 - failure of crash cooldown of steam generators
 - one airlock door open and seals on other door deflated
 - containment isolation failure
 - failure of dousing
- λ main coolant pump shaft failure
- + *i.e., Class 1 failure + safety system impairment (1 in 10,000 years)*



Class 5 - Examples

- λ small and large LOCA and, in turn:
 - loss of Emergency Core Coolant injection
 - heat transport system loop isolation failure
 - failure of crash cooldown of steam generators
 - one airlock door open and seals on other door deflated
 - containment isolation failure
 - failure of dousing
- λ turbine breakup, design basis tornado
- λ structural failures unless designed to appropriate standards
- λ *i.e., rare events + safety system impairment (less than 1 in 100,000 years)*



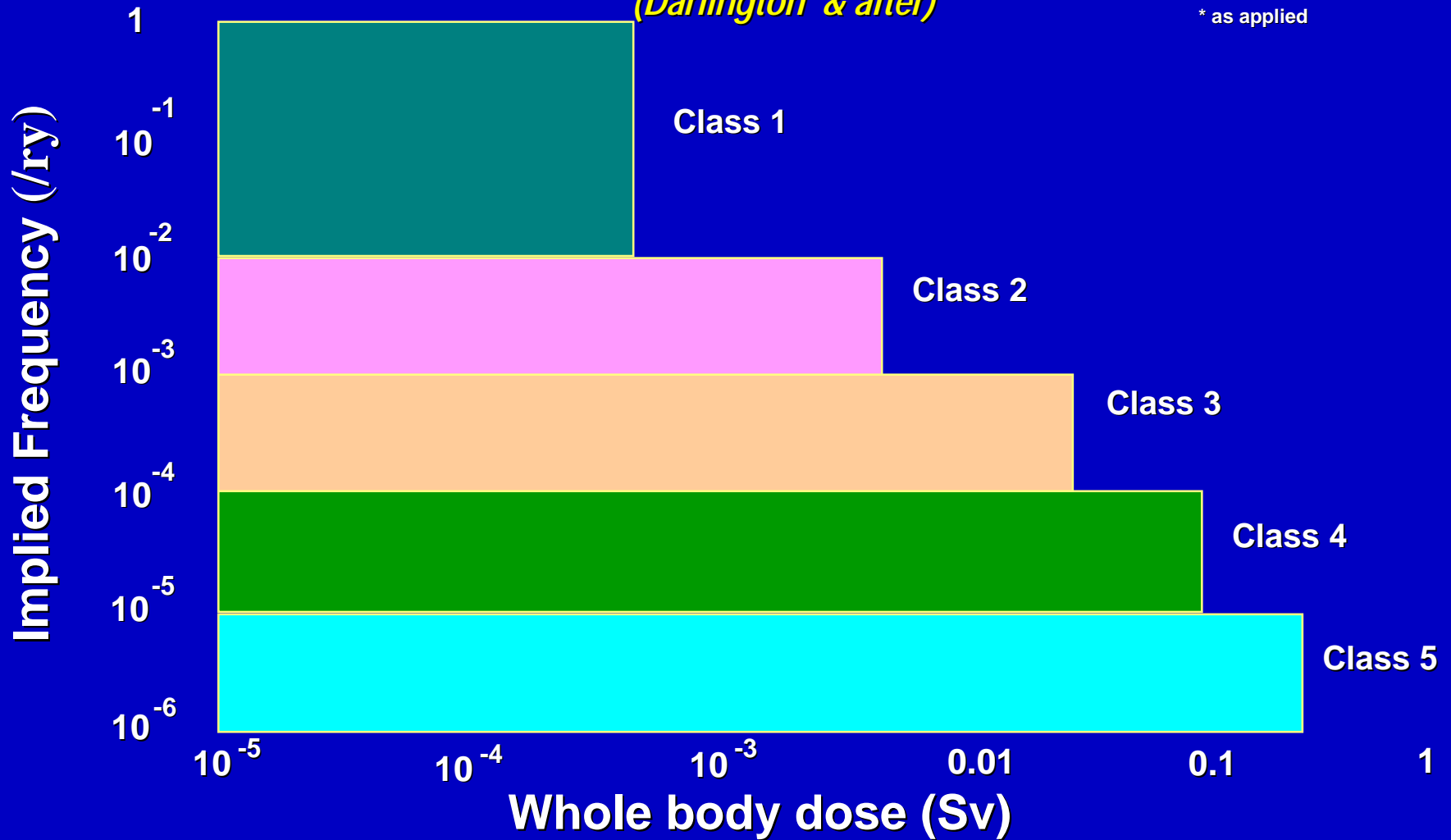
Specified Events Submitted for Information

- λ small and large LOCA and, in turn:
 - failure of all containment coolers
 - open airlock doors
- λ no acceptance criteria
- λ used by regulatory to see if there is a “cliff-edge” - i.e., sudden increase in consequences



AECB Consultative Document C-6 Criteria (Darlington* & after)

* as applied





Events Combined with Loss of Class IV Power

<i>Initiating Event Class</i>	<i>Event Class for “Initiating Event + Loss of Class IV Power”</i>
<i>1</i>	<i>3</i>
<i>2</i>	<i>4</i>
<i>3</i>	<i>5</i>
<i>4</i>	<i>5</i>
<i>5</i>	<i>5 or beyond design basis</i>



Techniques to Identify Other Accidents - 1

← pathways for movement of radioactivity

- identify locations of radioactivity
- identify events which would cause radioactivity to be relocated
- identify system failures which would lead to these events
- e.g., spent fuel bay: relocation due to overheating of fuel; overheating due to failure of bay cooling system

↑ system-by-system review

- examine failure of each process system in turn to see its effects
- e.g., heat transport system: loss of coolant, loss of flow



Techniques to Identify Accidents - 2

→ Probabilistic Safety Assessment

- use of fault-trees to define frequency of top events
- use of event trees to define required mitigating systems

λ PSA now the method of choice

λ no cutoff stated explicitly in C-6 but in practice do not consider events or event combinations below $\sim 10^{-6}$ per year

λ some exceptions: large LOCA + loss of Emergency Core Cooling is Design Basis but estimated frequency is 10^{-8} per year



Why is CANDU Accident Analysis So Complex?

- λ CANDU has more process systems (moderator)
- λ requirement to look at event combinations which are beyond design basis in most other countries
 - most of the accident analysis consists of multiple failures
 - in other countries, they would be in the PSA only, not in the design basis
- λ even for single events, onus is on designer to show the set of accidents is complete
 - he does not just take the list given by the regulator



Summary

- λ CANDU accident analysis does not stop at single initiating events, but considers double and triple event combinations
- λ in many ways it is like a Level 2 PSA done according to deterministic rules
- λ the disadvantage is complexity; the advantage is that the design examination is very thorough